# **Fire Behavior Modeling Conclusions and Recommendations**

- The fire behavior modeling conclusions and recommendations presented herewith are summarized from the following comprehensive analyses and reports, both of which can be found at Appendix M of the Draft Environmental Impact Report (Wildfire Risk Analysis) for each project:
  - Wildland Fire Evacuation Risk Report Fire Behavior The Village of Marble Valley Project, prepared by Firesafe Planning Solutions dated October 24, 2023
  - Wildland Fire Evacuation Risk Report Fire Behavior Lime Rock Project, prepared by Firesafe Planning Solutions dated November 1, 2023
  - Note: The modeling outputs, wind speed impacts, and development impacts shown on pages 5-7 of this document is one example only. Refer to the Wildland Fire Evacuation Risk Reports for the Village of Marble Valley and Lime Rock Valley for the complete analyses.
- A review of the expected fire behavior, using the worst-case scenarios, in the interface of the Marble Valley and Lime Rock Valley developments, indicates that the fire behavior could produce extreme fire behavior, and as such, risk reduction measures will be necessary.
- The configuration of the Project Site, the placement of the structures and features on the topography and the nature of the wildland fuels surrounding the project create conditions where the fire will travel at great speeds when wind, slope and fuel align BUT all of the access points are not impacted by fire at the same time.
- The fire behavior static modeling in this report with flame lengths of up to 55' under the worst-case scenario would be protected by compliance with the Fire Department fuel modification/defensible space standards. Fuel modification/defensible space is designed to reduce and change the fuel types as the combustible vegetation gets closer to the structure. As a "rule of thumb," two times the maximum flame length is adequate protection from radiant heat in a hardened structure. These distances also protect from direct flame contact (a distance greater than the flame length by a factor of two) and convected heat (less impactful than the radiant heat distance as discussed previously). The structure hardening (including ember intrusion projection) protects from embers and brands which may travel long distances under worst-case conditions. Fire burning through the development area is improbable.
- Risk reduction measures are required by the State and Local fire/building regulations, fire department standards, and guidelines, and by risk reduction measures already considered and applied by the development review process.



24-1388 | 1 of 7

## **Fire Behavior Modeling Conclusions and Recommendations**

- Fire behavior modeling predicts that there will be varied timeframes for evacuation of the Project Site under fire scenarios where the fire is burning into the community from an adjacent area. Each scenario has its own set of parameters.
- Where fires are initialized within the Project Site or near its boundary, the fire incident command and control may have to determine if the population will be moved or "sheltered in place."
- The proposed community with its increased built-in fire protection features (defensible space, fuel modification, hardening of the structures and required maintenance), placement of the structures on the topography, overall orientation to the fuels, wind, and slope and nested (safe center) configuration would be a candidate for a "shelter in place" decision. While "shelter in place" is never a first option, history shows us that moving populations, once the fire has arrived, has increased risk, and should not be attempted when safe alternatives exist.
- It has been determined that, with the implementation of the risk reduction measures set forth in this report, the proposed development areas set forth as project configurations will have a less than significant impact from the wildland fire-related issues raised under the AG Guidelines, as well as under CEQA Guidelines Appendix G, Section XX Wildfire.



24-1388 | 2 of 7

2





24-1388 I 3 of 7

### **Modeling Assumptions:**

- 1. Moisture Scenario will be 3, 4, 5, 30, 50 (extreme)
- 2. Wind will be assumed to be from:
  - a. N, NNE, NE at 45 mph
  - b. SE, SSE, S, SSW, SW at 65 mph
- 3. Fuel models to be used
  - a. LCP\_LF2022\_FBFM40\_220\_CONUS
  - b. No modifications have been done to any layers
- 4. Development area are used as fire barriers due to fuel modification and defensible space protection. Community burn through is not expected.
- 5. Fire scenario will be with sustained winds (no diurnal effect)
- 6. No fuel conditioning is used with worst-case moisture scenario
- 7. Arrival Times are shown to eight hours, but fire scenario is unlimited
- 8. Foliar Moistures are assumed to be 100
- 9. Crown Fire Calculation Method is set to Finney (2004)
- 10. Spotting Probability is set to 0.99
- 11. Spotting Delay is set to 0
- 12. Fuels have not been adjusted to any disease or drought impacts
- 13. Slopes and Aspects have not been adjusted in the development area (barrier file adjusts this to some degree)

Inputs:	SURFACE						
	Description	69-62 -	Μ	Marble Val.	ley Fuel C	omparison	
Fuel/Ve	egetation, Surface/Unders	story		0	-1		
E-1M	Fuel Model		gri, gr	2, gr4, g	sı, gsz, s	nz, sn5, s	
Fuel Moisture			2				
1-h Fuel Moisture %			<u> </u>	3			
10-h Fuel Moisture %			5	5			
1	Live Herbaceous Fuel Moistur	re %	30	30			Fuel Mo
	Live Woody Fuel Moisture	%	50	50			101
Weathe	er vood y 1 de 1 violstale	70					102
	20-ft Wind Speed (upslope)	mi/h	0, 30,	0. 30. 40. 50. 65			104
	Wind Adjustment Factor		0.5	0.5			121
Terrain	1		-				122
	Slope Steepness	%	50				142
							145
							147
		Marbla	Valley Engl	Comparin	an		164
		wiarbie V	valley Fuel	comparis	on		181
			Head Fire				182
		Surface	e Fire Flame	Length (ft)			183
١							184
)	Fuel		20-ft Wind Speed (upslope)				185
	Model			mi/h			186
		0	30	40	50	65	188
	grl	1.8	2.6	2.6	2.6	2.6	14
	gr2	4.2	11.6	11.6	11.6	11.6	15
	gr4	7.8	25.1	30.1	33.7	33.7	16
	gs1	3.5	11.1	11.7	11.7	11.7	17
	gs2	5.1	16.1	19.2	22.2	23.4	
	sh2	4.8	13.5	16.0	18.2	21.4	
	sh5	12.2	36.8	42.5	47.7	54.7	
	sh7	12.0	34.6	39.9	44.7	51.2	
	tu4	5.5	17.3	21.1	24.7	29.8	
	tu5	7.3	18.2	20.8	23.2	26.5	
	tll	0.6	0.8	0.8	0.8	0.8	
	tl2	0.8	1.4	1.4	1.4	1.4	
	tl3	1.0	1.9	1.9	1.9	1.9	
	tl4	1.3	2.8	2.8	2.8	2.8	
	115	1.9	5.4	6.0	6.0	6.0	
	tl6	2.5	7.2	8.6	10.0	10.5	
	118	2.5	9 5	10.1	11 5	13 6	
	SCAL14	0.0	25.3	29.1	30 6	34.0	
	SCAL14	9.8	20.2	20.1	30.6	34.0	
	SCALIS	7.3	20.1	22.9	25.3	28.6	
	SCAL16	9.6	27.3	31.1	34.5	39.0	
	SCAL17	6.5	20.2	23.9	27.3	32.1	

#### **Fire Modeling Inputs**

Label	Description			
gr1	Short, sparse, dry climate grass (D)			
gr2	Low load, dry climate grass (D)			
gr4	Moderate load, dry climate grass (D)			
gsl	Low load, dry climate grass-shrub (D)			
gs2	Moderate load, dry climate grass-shrub (D)			
sh2	Moderate load, dry climate shrub (S)			
sh5	High load, dry climate shrub (S)			
sh7	Very high load, dry climate shrub (S)			
tu4	Dwarf conifer understory (S)			
tus	Very high load, dry climate timber-shrub (S)			
t11	Low load, compact conifer litter (S)			
t12	Low load broadleaf litter (S)			
t13	Moderate load conifer litter (S)			
t14	Small downed logs (S)			
t15	High load conifer litter (S)			
t16	High load broadleaf litter (S)			
t18	Long-needle litter (S)			
SCAL14	Manzanita			
SCAL15	Chamise 1			
SCAL16	North Slope Ceanothus			
SCAL17	Chamise 2			



24-1388 | 4 of 7

4



#### 24-1388 | 5 of 7



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	EVA 10	EVA-2n	EVA-3n	EVA·4n	EVA-5n
	D.	D.	a	n	b
t i	1000	270+0	40N/A0	Nonen	Nonep
0	N/AD	180=	N/A¤	None	NoneD
E	100¤	27010	40-N/An Nonen		None¤
6	900	400+□	45N/Λ¤	None	None
1	N/A¤	360¤	N/Ap Nonep		None¤
1	1050	None	45-N/An Nonen		Nonen
E	85¤	None¤	45N/A0	None	Nonett
1	N/A¤	210¤	N/A¤	N/A= None=	
r	90□	None	55 · ·N/A□ None□		None
ſ	110¤	None	65¤	65¤ None¤	
£.	N/A¤	230□	N/An Nonen		None
	110¤	None	65¤ None¤		None¤
E	None¤	200¤	N/Aq	360 I¤	360+¤
8	N/A¤	2200	N/A¤	None	Noneta

### Modeling Outputs



24-1388 | 6 of 7



24-1388 | 7 of 7